Learned rotationally symmetric diffractive achromat for full-spectrum computational imaging: supplement

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This document provides supplementary information to *Learned Rotationally Symmetric Diffractive Achromat for Full-Spectrum Computational Imaging*. We provide detailed derivation of the rotationally symmetric point spread function (PSF) model. We also provide the additional details about the utilized image recovery neural network and the fabrication. In addition, we provide the comparison of the proposed Res-Unet recovery with model-based methods, that under different loss function configurations, and that designed with the Zernike base parameterization, as well as extra experimental results captured with our fabricated DA but using a machine vision sensor.

1. ROTATIONALLY SYMMETRIC PSF MODEL

In the following, we describe the details of deriving Eq. 3 in main text. We first rewrite Eq. 1 in main text as:

$$PSF(x, y, \lambda) = \left| \frac{1}{\lambda f} e^{\pi \lambda f^2} \right| \left| \int \int P(s, t, \lambda) e^{i \pi \lambda f^2 + \pi \lambda f^2} dsdt \right|^2.$$  \hspace{1cm} (S1)

By substituting $k = \frac{2\pi}{\lambda}$ and assuming $f_x = \frac{y}{f}$ and $f_y = \frac{x}{f}$, Eq. S1 can be expressed as:

$$PSF(f_x, f_y, \lambda) = \left| \frac{1}{\lambda f} e^{i \pi \lambda f^2 (f_x^2 + f_y^2)} \right| \left| \int \int P(s, t, \lambda) e^{i 2\pi (f_x s + f_y t)} dsdt \right|^2.$$  \hspace{1cm} (S2)

Next, we convert the coordinate system from the Cartesian to polar by substituting $f_x = r \cos \phi, f_y = r \sin \phi, s = r \cos \theta, t = r \sin \phi$. Accordingly, we further rewrite Eq. S2 as:

$$PSF(r, \theta, \lambda) = \left| \frac{1}{\lambda f} e^{i \pi \lambda f^2} \int_0^\infty \int_0^{2\pi} P(r, \phi, \lambda) e^{i \pi r^2} e^{-2\pi r \cos(\theta - \phi)} r d\phi dr \right|^2.$$  \hspace{1cm} (S3)

by assuming the height profile of DA is rotational symmetric, we observe the polar version of the pupil function $P(r, \phi, \lambda)$ is...
independent with $\phi$. Then, Eq. S3 can be rewritten as:

$$PSF(\rho, \lambda) = \left| \frac{1}{\lambda f} e^{i \pi f \rho^2} \int_0^{\infty} r P(r, \lambda) e^{\hat{\varphi} r^2} e^{-i 2 \pi \sigma \rho \cos(\theta - \phi)} \, rd\rho \right|^2$$

$$= \left| \frac{1}{\lambda f} e^{i \pi f \rho^2} \int_0^{2\pi} r P(r, \lambda) e^{\hat{\varphi} r^2} e^{-i 2 \pi \sigma \rho \cos(\theta - \phi)} \, rd\rho \right|^2$$

$$= \left| \frac{1}{\lambda f} e^{i \pi f \rho^2} \int_0^{2\pi} r P(r, \lambda) e^{\hat{\varphi} r^2} \, rd\rho \right|^2$$

$$= \left( \frac{2\pi e^\frac{i}{\lambda f} \hat{\lambda}(\rho)}{\lambda f} \right)^2 \int_0^{2\pi} r P(r, \lambda) e^{\hat{\varphi} r^2} j_0(2\pi \rho \sigma) \, dr \right|^2,$$

where $j_0$ is the 0th order of Bessel function of the first kind.

Since the DA is discretized as a number of concentric rings with a ring width of $d$, as illustrated in Fig. 2 in main text, the term $P(r, \lambda) e^{\hat{\varphi} r^2}$ can be decomposed to many $\text{circ}$, written as:

$$P(r, \lambda) e^{\hat{\varphi} r^2} \approx P(r, \lambda) e^{\hat{\varphi} \circ \rho} \left( \frac{r}{r_1} \right) + \sum_{m=2}^{\infty} P(r_m, \lambda) e^{\hat{\varphi} \circ \rho} \left( \frac{r}{r_m} \right) - (S5)$$

$$P(r_m, \lambda) e^{\hat{\varphi} \circ \rho} \left( \frac{r}{r_m} \right),$$

where $r_m = m d$ (for $m = 1, 2, \ldots$), $d$ is the feature size of DA. The approximation of Eq. S5 is accuracy when the ring sampling $d$ sufficiently fine to accurately approximate the additional phase term $e^{\hat{\varphi} \circ \rho}$ by $\hat{\varphi} \circ \rho_m$, for example $d \leq \frac{\lambda}{NA}$ [1], where NA is the numerical number of the DA. The $\text{circ}$ is the unit circ function, defined as:

$$\text{circ}(r) = \begin{cases} 1, & |r| \leq 1 \\ 0, & |r| > 1 \end{cases}. \quad (S6)$$

By substituting Eq. S5 into Eq. S4, we derive the notations $G(r, \lambda), K(r, \lambda)$ to represent $P(r, \lambda) e^{\hat{\varphi} \circ \rho}$ and $\frac{2\pi e^\frac{i}{\lambda f} \hat{\lambda}(\rho)}{\lambda f}$, respectively, expressed as:

$$PSF(\rho, \lambda) = \left| K(r, \lambda) \left[ \int_0^{\infty} \rho G(r, \lambda) \text{circ} \left( \frac{r}{r_1} \right) j_0(2\pi \rho \sigma) \, dr \right] + \sum_{m=2}^{\infty} G(r_m, \lambda) \left[ \int_0^{\infty} \rho \text{circ} \left( \frac{r}{r_m} \right) - (S7) \right] \right|^2.$$  

Eq. S7 can be further expressed as:

$$PSF(\rho, \lambda) = \left| K(r, \lambda) \left[ G(r_1, \lambda) \int_0^{r_1} r j_0(2\pi \rho \sigma) \, dr + \sum_{m=2}^{\infty} G(r_m, \lambda) \right| \int_0^{r_m} r j_0(2\pi \rho \sigma) \, dr - \int_0^{r_{m-1}} r j_0(2\pi \rho \sigma) \, dr \right|^2$$

$$= \left| K(r, \lambda) \left[ G(r_1, \lambda) \frac{1}{2\pi \rho} r_1 j_1(2\pi \rho r_1) + \frac{1}{2\pi \rho} \sum_{m=2}^{\infty} G(r_m, \lambda) \right| r_m j_1(2\pi \rho r_m) - r_{m-1} j_1(2\pi \rho r_{m-1}) \right|^2 \right|^2$$

$$= \left| \frac{2\pi e^\frac{i}{\lambda f} \hat{\lambda}(\rho)}{\lambda f} \sum_{m=1}^{\infty} P(r_m, \lambda) e^{\hat{\varphi} \circ \rho} H(r_m, \rho) \right|^2,$$

where $H(r_m, \rho)$ is expressed as:

$$H(r_m, \rho) = \begin{cases} \frac{1}{2\pi \rho} \left[ r_m j_1(2\pi \rho r_m) - r_{m-1} j_1(2\pi \rho r_{m-1}) \right], & m > 1 \\ \frac{1}{2\pi \rho} r_1 j_1(2\pi \rho r_1), & m = 1 \end{cases}. \quad (S9)$$

2. DETAILS OF IMAGE RECOVERY NEURAL NETWORK

The configuration details of the base unit of the image recovery neural network are presented in Tab. S1.

3. ABLATION STUDY OF LOSS FUNCTIONS

We provide alternative results implemented with the $\ell_1$ loss and SSIM loss. We use the same training set, parameters, and network configure except the loss function is changed to $\ell_1$ loss and SSIM loss. We assess 15 test images using peak signal-to-noise ratio (PSNR), structural similarity index (SSIM), and spectral angular mapper (SAM) [2]. The Gaussian noise with $\sigma=0.003$ is added to all sensor measurements. Table S2 summarizes the average PSNR, SSIM, SAM and Fig. S1 shows an example selected from the test set. We observe that the $\ell_2$ loss leads to better results (with the average PSNR improvements of 0.50 dB).
Table S2. Quantitative evaluation of the averaged PSNR (dB), SSIM, and SAM over 15 test images resolved with the network trained with different loss functions.

<table>
<thead>
<tr>
<th>Loss</th>
<th>$\ell_1$</th>
<th>SSIM</th>
<th>$\ell_2$</th>
</tr>
</thead>
<tbody>
<tr>
<td>Recovery</td>
<td>32.53 / 0.886 / 0.07</td>
<td>32.59 / 0.896 / 0.07</td>
<td>33.09 / 0.892 / 0.07</td>
</tr>
</tbody>
</table>

4. ADDITIONAL SIMULATION RESULTS

Comparison with alternative image recovery algorithms

We show the comparison among different image recovery methods. Table S3 summarizes the averaged PSNR and Fig. S2 visualizes several examples selected from the test set. We observe that the score of Wiener filtering is quite low since the recovered images are noisy (see Fig. S2), although the details and the color fidelity look good. After further applying a learning-based multi-layer perceptron (MLP) approach [3], the score shows a gain of 3.33 dB. However, this score is still significantly lower than that of images recovered by the proposed Res-Unet (see Fig. S2). These results validate that the proposed Res-Unet is capable of preserving high-fidelity scene details while suppressing noise in the meantime.

Table S3. Quantitative evaluation of averaged PSNR (dB) over 15 test images resolved using different recovery algorithms.

<table>
<thead>
<tr>
<th></th>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>Recovery image</td>
<td>23.38</td>
<td>26.71</td>
<td>33.09</td>
</tr>
</tbody>
</table>

Comparison under different noise levels

We provide additionally results for the performance assessment of the diffractive achromat (DA) designs with noise levels $\sigma=0.006$ and $\sigma=0.011$. Table S4 summarizes the averaged PSNR and Fig. S2 visualizes an example selected from the test set. We observe that the proposed DA, in tandem with the Res-Unet, obtains the best performance under noise levels of 0.003 and 0.006. Note that this performance improvement becomes less noticeable when the noise level is increased. Specifically, the PSNR improvement decreases from 1.3 dB to 0.16 dB, and the SSIM improvement decreases from 0.015 to N/A. That said, our current end-to-end design framework may only show superior results when deriving DAs for full-spectrum applications under low and median noise levels, which are very reasonable for state-of-the-art sensors.

Table S4. Quantitative evaluation of averaged PSNR (dB), SSIM, and SAM over 15 test images resolved with different lens designs and Res-Unet recovery algorithms at different noise levels.

<table>
<thead>
<tr>
<th>Noise Level</th>
<th>Fresnel Lens</th>
<th>Reference DA</th>
<th>Proposed DA</th>
</tr>
</thead>
<tbody>
<tr>
<td>$\sigma=0.003$</td>
<td>25.78 / 0.804 / 0.12</td>
<td>31.79 / 0.877 / 0.08</td>
<td>33.09 / 0.892 / 0.07</td>
</tr>
<tr>
<td>$\sigma=0.006$</td>
<td>25.46 / 0.786 / 0.13</td>
<td>31.35 / 0.865 / 0.08</td>
<td>32.30 / 0.874 / 0.07</td>
</tr>
<tr>
<td>$\sigma=0.011$</td>
<td>24.78 / 0.734 / 0.15</td>
<td>30.38 / 0.840 / 0.08</td>
<td>30.54 / 0.828 / 0.08</td>
</tr>
</tbody>
</table>

Comparison with a hyperspectral diffractive lens

We have compared with the DOE designed to better estimate (e.g., hyperspectral imaging) the spectral information as in [4]. We design the hyperspectral DOE using the method described in the relevant work [4] with a focal length of 50 mm and an aperture diameter of 8 mm. The design spectrum range is from 420 nm to 699 nm. We use the same training set and parameters to train the image recovery Res-Unet for this hyperspectral DOE. We assess 15 test images using PSNR, SSIM, and SAM. The Gaussian noise with $\sigma=0.003$ is added to all sensor measurements. Table S5 summarizes the average PSNR, SSIM, SAM and Fig. S4 shows an example selected from the test set. We observe that the proposed DA obtains better results (with the averaged PSNR and SAM improvements of 8.82 dB and 0.06, respectively). As shown in the right bottom of Fig. S4, the hyperspectral DOE is designed to distinguish the spectral PSFs as much as possible. Thus, the resulting blur is very sensitive to the aperture diameter.
Fig. S3. Selected examples of the assessment of three lens designs with different noise levels in simulation. We show the recovery results of the Res-Unet. The inset values indicate the PSNR (dB) and SSIM.

In our case, the blur size of the PSFs goes up to approximately 3 mm, which causes image recovery algorithms failing to resolve a full-spectrum image. This means for a practical DOE with an aperture diameter of 8 mm, their design framework fails to obtain high-fidelity color images.

Table S5. Quantitative evaluation of averaged PSNR (dB), SSIM, and SAM over 15 test images resolved with different lens designs and different ResUnet recovery algorithms.

<table>
<thead>
<tr>
<th>Type</th>
<th>Hyperspectral DOE</th>
<th>Proposed DA</th>
</tr>
</thead>
<tbody>
<tr>
<td>Measurement</td>
<td>17.77 / 0.613 / 0.19</td>
<td>19.90 / 0.657 / 0.14</td>
</tr>
<tr>
<td>Recovery</td>
<td>24.27 / 0.714 / 0.13</td>
<td>33.09 / 0.892 / 0.07</td>
</tr>
</tbody>
</table>

Comparison with a DOE designed with alternative rotationally symmetric base representation We choose the 16 circularly symmetric Zernike bases among the first 150 Zernike terms. For a fair comparison, we use the same training set, parameters, and network structure to learn the lens. We assess on 15 test images using the PSNR, SSIM, and SAM. The Gaussian noise with $\sigma=0.003$ is added to all sensor measurements. Table S6 summarizes the averaged PSNR, SSIM, SAM, and Fig. S5 shows an example selected from the test set. Although the learned lens with Zernike basis shows the best result, it is a refractive lens because of its continual surface representation. That said, the maximum height of the lens is around 284 $\mu$m, which is 142 $\times$ as that of the...
designed DOE. If we warp the learned Zernike lens to the same height of the proposed DA, as shown in the middle of Fig. S5, the warped Zernike lens becomes a Fresnel lens, further leading to poor performance.

Fig. S5. Selected examples of the assessment between the proposed DA and the DOE designed with alternative rotationally symmetric basis. The inset values indicate the PSNR (dB) and SSIM. Warping means to warp the learned Zernike lens to the same height of the proposed DA.

Table S6. Quantitative evaluation of averaged PSNR (dB), SSIM, and SAM, over 15 test images resolved with different lens designs and ResUnet recovery algorithms.

<table>
<thead>
<tr>
<th>Type</th>
<th>Zernike</th>
<th>Zernike (warped)</th>
<th>Proposed</th>
</tr>
</thead>
<tbody>
<tr>
<td>Measurement</td>
<td>27.89 / 0.803 / 0.88</td>
<td>19.58 / 0.647 / 0.17</td>
<td>19.90 / 0.657 / 0.14</td>
</tr>
<tr>
<td>Recovery</td>
<td>36.45 / 0.9643</td>
<td>17.07 / 0.6656</td>
<td>33.23 / 0.9156</td>
</tr>
</tbody>
</table>

5. PROTOTYPING

Fabrication details As shown in Fig. S6, the designed DOEs are fabricated using the imprinting lithography technique. Specifically, the positive photoresist (AZ-1512, MicroChemicals) is spun on a titanium-coated glass substrate and is patterned by a direct-write optical grayscale lithography machine (MicroWriter ML3, Durham Magneto Optics). Then, the photoresist is developed with a base developer (MF-319, Microposit) and is used as a mold to replicate its pattern on polydimethylsiloxane (PDMS, SYLGARD 184, Dow). PDMS, a two-part polymer, is mixed at the standard ratio of 10:1 and degassed in the vacuum. The mixed PDMS is cured at room temperature for three days with the master mold to make the elastomeric mold. The circular aperture is fabricated with a light-blocking chromium-gold-chromium tri-layer (50 nm / 100 nm / 50 nm) on a 3 mm thick float glass substrate (30-773, Edmund Optics) through the lift-off process. Then, a drop of optically clear UV-curable resin (NOA61, Norland Products) is put between the PDMS mold and the glass substrate and cured with a mercury vapor lamp after aligning the pattern with the circular aperture. Finally, the PDMS mold is gently peeled off to form a patterned clear resin layer on the glass substrate.

Fig. S6. Fabrication process of our proposed DA.

Prototype camera and experiment setup As shown in Fig. S7, the fabricated DA is mounted to a 1-inch stand tube and then attached to a Canon T5i DSLR camera body via a customized printed holder. We capture the PSF of the fabricated DA using a white LED light source and a 35 µm pinhole attached in front. The distance between the light source and the front surface of the fabricated DA is 3 m, and we slightly adjust the gap between the DA and DSLR sensor to focus at the light source. To obtain a PSF with a high dynamical range, we capture PSFs with four integration settings, including 100 ms, 200 ms, 400 ms, and 800 ms, and then merge them. The measured PSF is used to refine the image recovery neural network.

Fig. S7. Photographs of the prototype lens and the experimental setup using a DSLR camera body.

Image recovery network refining In Fig. S8, we show the selected results with and without the refining of the image recovery network using the measured PSFs. It is clear that the refining step leads to an increase of performance. Here, we use a new RGB dataset [5] since we have replaced the spectral PSFs at 31 wavelengths with the RGB PSF. 20 images are used for the evaluation and the remaining for refining. Finally, we assess on 20 images with the Gaussian noise level of 0.005 and observe that both the PSNR and SSIM have indicated the increase from 27.88 dB and 0.774 to 31.03 dB and 0.793, respectively. The visual performance, regarding color performance and noise issue, has been significantly improved as well.
6. ADDITIONAL CAPTURED RESULTS

To comprehensively verify the achromatic performance of our designed DA, we evaluate our designed DA on another machine vision sensor (Pointgrey Grasshopper3 USB3) that has 1,900 × 1,200 pixels with the pixel pitch of 5.9 µm. We reimplement the PSF calibration and refine the image recovery network, as mentioned in the main text. Figure S9 shows several results that captured in the real world where the images are displayed on a display monitor. The details and color are well resolved, indicating that our jointly designed diffractive lens suits well over different spectral response curves of sensors due to it is robust achromatic behavior.

REFERENCES


