# **CHAPTER 7 BEAM DEFLECTIONS DUE TO BENDING**

## EXERCISE 33, Page 156

**1.** Obtain an expression for the deflection y at any distance x from the left end of the uniform section beam of shown.





w = 2 = x/4

Taking moments about B gives:

$$R_A \times 4 = 2 \times 4 \times 2 + \frac{1}{2} \times 4 \times 1 \times \frac{1}{3} \times 4$$
$$= 16 + 2.667$$

i.e.

$$R_A = 4.667 \text{ kN}$$

Resolving vertically gives:

$$R_A + R_B = \frac{(2+3)}{2} \times 4 = 10$$
 1

i.e.

$$R_B = 10 - 4.667 = 5.333 \text{ kN}$$

$$EI\frac{d^2y}{dx^2} = 4.667x - \frac{2 \times x}{2} \times \frac{2}{3}x - \frac{1}{2}\left(2 + \frac{x}{4}\right) \times x \times \frac{1}{3} \times x$$
$$= 4.667x - 0.667x^2 - \frac{1}{6}\left(2x^2 + \frac{x^3}{4}\right)$$
$$= 4.667x - 0.667x^2 - 0.333x^2 - 0.0417x^3$$

i.e.

$$EI\frac{d^2y}{dx^2} = 4.667x - x^2 - 0.0417x^3$$

$$EI\frac{dy}{dx} = \left(\frac{4.667}{2}\right)x^2 - \frac{1}{3}x^3 - \left(\frac{0.0417}{4}\right)x^4 + A$$

i.e.

$$EI\frac{dy}{dx} = 2.333x^2 - 0.333x^3 - 0.01043x^4 + A$$

$$EIy = \left(\frac{2.333}{3}\right)x^3 - \left(\frac{0.333}{4}\right)x^4 - \left(\frac{0.01043}{5}\right)x^5 + Ax + B$$

(1)

i.e.

At 
$$x = 0$$
,  $y = 0$ , hence, ***B*** = **0**

At x = 4, y = 0,

$$0 = 49.79 - 21.32 - 2.14 + 4A$$

from which, A = -26.33/4 = 6.583

i.e. from equation (1),

y = 
$$\frac{1}{EI}$$
 (0.778x<sup>3</sup> - 0.0833x<sup>4</sup> - 2.086×10<sup>-3</sup>x<sup>5</sup> - 6.583x)

 $EIy = 0.778x^3 - 0.0833x^4 - 0.002086x^5 + Ax + B$ 

2. Determine the value of the reactions and end fixing moments for the uniform-section beam shown. Hence, or otherwise, obtain an expression for the deflection y at any distance x from the left end of the beam by the double integration method.



$$EI\frac{d^2y}{dx^2} = R_A x - M_A - 0.667x^2 - 0.333x^2 - 0.0417x^3$$

i.e. 
$$EI\frac{d^2y}{dx^2} = R_A x - M_A - x^2 - 0.0417x^3$$

and

$$EI\frac{dy}{dx} = \frac{R_A x^2}{2} - M_A x - \frac{x^3}{3} - \frac{0.0417x^4}{4} + A$$
$$EI\frac{dy}{dx} = 0.5 R_A x^2 - M_A x - 0.333x^3 - 0.01043x^4 + A$$
$$EIy = \frac{0.5R_A x^3}{3} - \frac{M_A x^2}{2} - \frac{0.333x^4}{4} - \frac{0.01043x^5}{5} + Ax + B$$

i.e.

and

$$EIy = 0.167 R_A x^3 - 0.5 M_A x - 0.0833 x^4 - 2.086 \times 10^{-3} x^5 + Ax + B$$
(i)

At 
$$x = 0$$
,  $y = 0$  hence,  $\boldsymbol{B} = \boldsymbol{0}$ 

At x = 0,  $\frac{dy}{dx} = 0$ , hence, A = 0

Therefore, from equation (i),

$$y = \frac{1}{EI} \{ 0.77 x^3 - 1.62 x^2 - 0.0833 x^4 - 2.086 \times 10^{-3} x^5 \}$$

At x = 4,  $\frac{dy}{dx} = 0$ ,

hence,  $0 = 8 R_A - 4 M_A - 21.31 - 2.67$ 

$$8 R_{\rm A} - 4M_{\rm A} - 24 = 0 \tag{1}$$

At x = 4, y = 0,

i.e.

hence, 
$$0 = 10.69 R_A - 8M_A - 21.43 - 2.13$$
  
i.e.  $5.345 R_A - 4M_A - 11.73 = 0$  (2)

Taking equation (2) from equation (1) gives:

$$2.655 R_A - 12.27 = 0$$

from which,  $R_A = 4.62 \text{ kN}$ 

Substituting equation (3) into equation (1) gives:

$$36.97 - 4 M_A - 24 = 0$$

from which,  $M_A = 3.24$  kN m

$$R_B = 5.38 \text{ kN}$$

Taking moments about B gives:

$$M_B + 4.62 \times 4 = 3.24 + 2 \times 4 \times 2 + \frac{1}{2} \times 4 \times 1 \times \frac{1}{3} \times 4$$

i.e.

$$M_B = -18.48 + 3.24 + 16 + 2.67$$

from which,  $M_B = 3.43$  kN m

**3.** Obtain an expression for the deflection y at any distance x from the left end of the uniform section beam shown.





$$w = \frac{3x}{l} = \frac{3x}{4} = 0.75x \text{ kN/m}$$

Taking moments about *B* gives:

$$R_1 \times 4 \,\mathrm{m} = 3 \,\frac{\mathrm{kN}}{\mathrm{m}} \times \frac{4 \,\mathrm{m}}{2} \times \frac{1}{3} \times 4 \,\mathrm{m}$$

i.e. 
$$4R_1 = 8$$
 and  $R_1 = 2$  kN

Resolving vertically gives:

 $R_1 + R_2 = \frac{3 \times 4}{2} = 6 \,\mathrm{kN}$ 

Hence,

$$R_2 = 6 - 2 = 4 \,\mathrm{kN}$$

$$EI\frac{d^2y}{dx^2} = M = R_1 \times x - w \times \frac{x}{2} \times \frac{x}{3}$$
$$= 2x - \frac{0.75x^3}{6}$$
$$EI\frac{dy}{dx} = 2\left(\frac{x^2}{2}\right) - \frac{0.75x^4}{4 \times 6} + A$$

i.e.

$$EI\frac{dy}{dx} = x^2 - 0.03125x^4 + A \tag{1}$$

 $\quad \text{and} \quad$ 

$$EIy = \frac{x^3}{3} - \frac{0.03125x^5}{5} + Ax + B$$
(2)

At 
$$x = 0$$
,  $y = 0$ , hence,  $B = 0$   
At  $x = 4$ ,  $y = 0$ , hence,  $0 = \frac{4^3}{3} - \frac{0.03125 \times 4^5}{5} + 4A$   
from which,  $4A = 6.4 - 21.33$   
and  $A = \frac{-14.93}{4} = -3.7325$ 

Hence,

$$EIy = \frac{x^3}{3} - \frac{0.03125x^3}{5} - 3.7325x$$
(3)

or 
$$y = \frac{1}{EI} (0.333x^3 - 0.00643x^5 - 3.7325x)$$

**4.** Determine the value of the reactions and end fixing moments for the uniform-section beam shown. Hence, or otherwise, obtain an expression for the deflection y at any distance x from the left end of the beam.





$$w = \frac{3x}{l} = \frac{3x}{4} = 0.75x \text{ kN/m}$$

Taking moments about *B* gives:

$$R_A \times 4 \,\mathrm{m} = M_A + 0.75 \times 4 \times \frac{4}{2} \times \frac{4}{3} - M_B$$

i.e.

$$4R_{A} = M_{A} + 8 - M_{B}$$

Resolving vertically gives:

$$R_A + R_B = \frac{3}{4} \times 4 \times \frac{4}{2} = 6$$

Hence,

$$R_B = 6 - R_A \tag{1}$$

$$EI\frac{d^{2}y}{dx^{2}} = R_{A} \times x - M_{A} - \frac{3}{4} \times x \times \frac{x}{2} \times \frac{x}{3}$$
$$= R_{A}x - M_{A} - \frac{0.75x^{3}}{6}$$
(2)

i.e.

$$EI\frac{d^2y}{dx^2} = R_A x - M_A - 0.125x^3$$
(2a)

$$EI\frac{dy}{dx} = R_A \left(\frac{x^2}{2}\right) - M_A x - \frac{0.125x^4}{4} + A$$
(3)

At 
$$x = 0$$
,  $\frac{dy}{dx} = 0$ , hence,  $A = 0$ 

At 
$$x = 4$$
,  $\frac{dy}{dx} = 0$ , hence,  $0 = R_A \left(\frac{4^2}{2}\right) - 4M_A - \frac{0.125(4)^4}{4}$ 

from which,

$$4M_{A} = 8R_{A} - 8$$

 $\quad \text{and} \quad$ 

$$M_A = 2R_A - 2 \tag{4}$$

From equation (3):

$$EIy = \frac{R_A x^3}{6} - \frac{M_A x^2}{2} - \frac{0.125 x^5}{20} + B$$
(5)

At x = 0, y = 0, hence, B = 0

At 
$$x = 4$$
,  $y = 0$ , hence,  $0 = \frac{R_A(4)^3}{6} - \frac{M_A(4)^2}{2} - \frac{0.125(4)^5}{20}$ 

i.e.

$$0 = 10.667 R_A - 8M_A - 6.4$$

or

$$M_A = 1.333 R_A - 0.8 \tag{6}$$

Equating equations (4) and (6) gives:

 $2R_A - 2 = 1.333R_A - 0.8$ 

i.e.

i.e.

 $0.667R_A = 1.2$ 

from which,

$$R_A = \frac{1.2}{0.667} = 1.8 \,\mathrm{kN} \tag{7}$$

From equation (1),  $R_B = 6 - R_A = 6 - 1.8$ 

i.e. 
$$R_B = 4.2 \,\mathrm{kN}$$
 (8)

Substituting equation (7) into equation (4) gives:

$$M_A = 2R_A - 2 = 2 \times 1.8 - 2$$
$$M_A = 1.6 \,\mathrm{kN} \,\mathrm{m} \tag{9}$$

At 
$$x = 4$$
,  $EI \frac{d^2 y}{dx^2} = M_B = 1.8 \times 4 - 1.6 - \frac{0.75(4)^3}{6}$  from equation (2a)

i.e. 
$$M_B = 7.2 - 1.6 - 8 = -2.4$$
 kN m

From equation (5), 
$$EIy = \frac{R_A x^3}{6} - \frac{M_A x^2}{2} - \frac{0.125x^5}{20} + B$$
  
i.e.  $y = \frac{1}{EI} \left( \frac{1.8x^3}{6} - \frac{1.6x^2}{2} - \frac{0.125x^5}{20} \right)$   
i.e.  $y = \frac{1}{EI} \left( 0.3x^3 - 0.8x^2 - 0.00625x^5 \right)$ 

## EXERCISE 34, Page 160

**1.** Determine the position (from the left end) and the value of the maximum deflection for the uniform-section beam shown.



Taking moments about B gives:

$$R_A \times 3.5 = 0.7 \times 1.5 \times 2.75$$

from which,  $R_A = 0.825 \text{ kN}$ 

$EI\frac{d^2y}{dx^2} = 0.825x - \frac{0.7x^2}{2}$	$+\frac{0.7}{2}(x-1.5)^2$
$EI\frac{dy}{dx} = 0.413x^2 - 0.117x^3 + A$	$+0.117 (x - 1.5)^3$
$EIy = 0.138x^3 - 0.0292x^4 + Ax + B$	$+0.0292 (x - 1.5)^4$

At 
$$x = 0$$
,  $y = 0$ , hence,  $B = 0$   
At  $x = 3.5$ ,  $y = 0$ ,  
hence,  $0 = 5.917 - 4.38 + 3.5A + 0.467$   
i.e.  $A = -0.573$   
For  $\delta$ ,  $\frac{dy}{dx} = 02$  between C and B  
 $0 = 0.413x^2 - 0.117x^3 - 0.573 + 0.117 (x^3 + 2.25x - 1.5x^2 - 3.375)$   
i.e.  $0 = 0.238x^2 + 0.263x - 0.967$   
and  $x = \frac{-0.263 \pm \sqrt{(0.263)^2 - 4(0.238)(-0.967)}}{2(0.238)} = 1.54 \text{ m}$   
EIy  $= 0.138x^3 - 0.0292x^4 + Ax + B$ 

and  $\delta = 0.543/EI$ 

2. Determine the deflections at the points C and D for the uniform-section beam shown, given that  $EI = 4300 \text{ kNm}^2$ .



w = x/6

Taking moments about B gives:

$$R_A \times 6 = 2 \times 2 + 5 + \frac{1}{2} \times 6 \times 1 \times \frac{2}{3} \times 6$$

from which,

$$R_A = 21/6 = 2.5 \text{ kN}$$

Taking moments about A gives:

$$R_B \times 6 + 5 = 2 \times 4 + \frac{1}{2} \times 6 \times 1 \times \frac{2}{3} \times 6$$

from which,

$$R_B = (20 - 5)/6 = 2.5 \text{ kN}$$

$$2.5 + 2.5 = \frac{1}{2} \times 6 \times 1 + 2 = 5$$

$EI\frac{d^2y}{dx^2} = 2.5x - \frac{1}{2} \times x \times \frac{x}{6} \times \frac{x}{3}$	-2 (x - 4)	$-5(x-5)^{0}$
$EI\frac{d^2y}{dx^2} = 2.5x - \frac{x^3}{36}$	-2(x-4)	$-5(x-5)^{0}$
$EI\frac{dy}{dx} = 1.25x^2 - \frac{x^4}{144} + A$	$-(x-4)^2$	- 5 (x - 5)
$EIy = 0.417x^3 - \frac{x^5}{720} + Ax + B$		

$-\frac{(x-4)^3}{3}$	$-\frac{5}{2}(x-5)^2$
5	2

At x = 0, y = 0, hence, B = 0

At x = 6, y = 0

Hence, 0 = 90 - 10.8 + 6A - 2.667 - 2.5

from which, A = -12.34

At x = 4,  $\delta_{c} = \frac{1}{4300} (26.69 - 1.422 - 49.36) = -5.60 \times 10^{-3} \text{ m}$ 

At 
$$x = 5$$
,  $\delta_{\mathbf{D}} = \frac{1}{4300} (52.1 - 4.34 - 61.7 - 0.3) = -3.32 \times 10^{-3} \text{ m}$ 

3. Determine the position and value of the maximum deflection of the simply supported beam shown, given that E I = 100 kN m<sup>2</sup>.



Taking moments about B gives:

$$R_A \times 4 + 2 = 2 \times 2 + 2 \times 1 \times 3$$

from which,

 $R_A = (10 - 2)/4 = 2 \text{ kN}$ 

$EI\frac{d^2y}{dx^2} = 2x - \frac{x^2}{2}$	$-2(x-2)+\frac{(x-2)^2}{2}$	$+2(x-3)^{0}$
$EI\frac{dy}{dx} = x^2 - \frac{x^3}{6} + A$	$-(x-2)^2 + \frac{(x-2)^3}{6}$	+2(x-3) (1)
$EIy = \frac{x^3}{3} - \frac{x^4}{24} + Ax + B$	$-\frac{(x-2)^3}{3} + \frac{(x-2)^4}{24}$	$+(x-3)^2$ (2)

At x = 0, y = 0, hence, **B = 0** 

At x = 4, y = 0,

hence, 0 = 21.33 - 10.667 + 4A - 2.667 + 0.667 + 1

from which,

$$A = -9.663/4 = -2.416$$

 $EI\frac{dy}{dx}3 = x^{2} - \frac{x^{3}}{6} - 2.416 - (x - 2)^{2} + \frac{(x - 2)^{3}}{6}4$ Therefore,

For maximum y,  $\frac{dy}{dx} = 05$ 

Try second 'span':

 $x^{2} - \frac{x^{3}}{6} - 2.416 - x^{2} + 4x - 4 + \frac{x^{3}}{6} - x^{2} + \frac{12x}{6} - \frac{8}{6} = 0$ 0

or

$$2.416 + 4x - 4 - x^2 + 2x - 1.33 =$$

i.e. 
$$-x^2 + 6x - 7.746 = 0$$

 $x = \frac{-6 \pm \sqrt{6^2 - 4(-1)(-7.746)}}{2(-1)} = \frac{-6 \pm 2.24}{-2}$ from which,

i.e.

As 
$$1.88 < 2$$
, the maximum deflection does not occur in the second 'span'.

x = 1.88 m

Consider first 'span':

 $0 = x^2 - \frac{x^3}{6} - 2.416$  6

Try x = 1.87,

then

0 = 3.497 - 1.0899 - 2.416 = 0

i.e.

(3)

For maximum deflection, substituting equation (3) into equation (2) gives:

x = 1.87 m (approximately)

$$\delta = \frac{1}{\mathrm{EI}} \left( 2.18 - 0.51 - 4.518 \right)^7$$

i.e.

 $\delta = -0.0285 \text{ m}$ 

4. The beam CAB is simply supported at the points A and B and is subjected to a concentrated load W at the point C, together with a uniformly distributed load w between the points A and B, as shown. Determine the relationship between W and wl, so that no deflection will occur at the point C.



$$R_A l = \frac{3Wl}{2} + \frac{wl^2}{2}$$

i.e.

$$R_{A} = \frac{3W}{2} + \frac{wl}{2} + R_{A} \left(x - \frac{l}{2}\right) - \frac{w}{2} \left(x - \frac{l}{2}\right)^{2}$$

$EI\frac{d^2y}{dx^2} = -Wx$	$+R_A\left(x-\frac{l}{2}\right)-\frac{w}{2}\left(x-\frac{l}{2}\right)^2$
$EI\frac{dy}{dx} = -\frac{Wx^2}{2} + A$	$+\frac{R_A}{2}\left(x-\frac{l}{2}\right)^2-\frac{w}{6}\left(x-\frac{l}{2}\right)^3$
$EIy = -\frac{Wx^3}{6} + Ax + B$	$+\frac{R_A}{6}\left(x-\frac{l}{2}\right)^3-\frac{w}{24}\left(x-\frac{l}{2}\right)^4$

At x = 0, y = 0, hence, B = 0

At x = l/2, y = 0,

hence,

$$0 = -\frac{Wl^3}{48} + \frac{Al}{2}$$
$$A = \frac{Wl^2}{24} 8$$

i.e.

At x = 3l/2, y = 0,

therefore,  $0 = -\frac{27Wl^3}{48} + \frac{3Wl^3}{48} + \frac{R_A}{6}l^3 - \frac{wl^4}{24}$ i.e.  $0 = -\frac{27W}{48} + \frac{3W}{48} + \frac{3W}{12} + \frac{wl}{12} - \frac{wl}{24}$ 

- i.e.  $0 = -\frac{W}{4} + \frac{wl}{24}$
- i.e.  $w = \frac{6W}{l}$

**5.** Determine the position (from the left end) and the value of the maximum deflection for the uniform-section beam shown.





Taking moments about *B* gives:

$$R_A \times 5 = 0.7 \times 2 \times 4$$

from which,

 $R_A = 5.6 / 5 = 1.12 \text{ kN}$ 

$$EI\frac{d^{2}y}{dx^{2}} = 1.12x - \frac{0.7x^{2}}{2} + \frac{0.7(x-2)^{2}}{2}$$

$$EI\frac{dy}{dx} = \frac{1.12x^{2}}{2} - \frac{0.7x^{3}}{6} + A + \frac{0.7(x-2)^{3}}{6}$$

$$EIy = \frac{1.12x^{3}}{6} - \frac{0.7x^{4}}{24} + Ax + B + \frac{0.7(x-2)^{4}}{24}$$

At 
$$x = 0$$
,  $y = 0$ , hence,  $B = 0$   
At  $x = 5$  m,  $y = 0$ , hence,  $0 = \frac{1.12(5)^3}{6} - \frac{0.7(5)^4}{24} + 5A + \frac{0.7(3)^4}{24}$ 

i.e. 0 = 23.333 - 18.229 + 5A + 2.363

i.e. 5A = 18.229 - 23.333 - 2.363 = -7.467

and A = -7.467/5 = -1.4934

The maximum deflection,  $\delta$ , occurs where  $\frac{dy}{dx} = 0$ 

Since

$$EI\frac{dy}{dx} = \frac{1.12x^2}{2} - \frac{0.7x^3}{6} + A + \frac{0.7(x-2)^3}{6}$$

i.e.

$$EI\frac{dy}{dx} = \frac{1.12x^2}{2} - \frac{0.7x^3}{6} + A + \frac{0.7(x-2)(x^2 - 4x + 4)}{6}$$

 $EI\frac{dy}{dx} = \frac{1.12x^2}{2} - \frac{0.7x^3}{6} + A + \frac{0.7(x^3 - 6x^2 + 12x - 8)}{6}$ i.e.

Hence, at maximum  $\delta$ ,  $0 = 0.56x^2 - 0.1167x^3 - 1.4934 + 0.1167x^3 - 0.7x^2 + 1.4x - 0.9333$ 

i.e. 
$$-0.14x^2 + 1.4x - 2.4267 = 0$$

Using a calculator or the quadratic formula,

$$x = 7.769$$
 (which is neglected) or 2.231 m

$$EIy = \frac{1.12x^3}{6} - \frac{0.7x^4}{24} + Ax + B + \frac{0.7(x-2)^4}{24}$$

i.e.

$$EIy = 0.1867x^3 - 0.029167x^4 - 1.4934x + 0.02917(x-2)^4$$

When 
$$x = 2.231$$
,  $\delta = \frac{1}{EI} \{ 0.1867(2.231)^3 - 0.029167(2.231)^4 - 1.4934(2.23) + 0.02917(0.231)^4 \}$   
=  $\frac{1}{EI} \{ 2.073 - 0.723 - 3.332 + 8.306 \times 10^{-5} \}$   
i.e.  $\delta = -\frac{1.98}{EI}$ 





Taking moments about *B* gives:

$$R_A \times 7 = \frac{1 \times 7}{2} \times \frac{7}{3} + 2 \times 2 + 5$$

$$= 8.167 + 4 + 5 = 17.167$$

from which,

 $R_A = 17.167 / 7 = 2.452 \text{ kN}$ 

Resolving vertically gives:

$$R_A + R_B = \frac{1 \times 7}{2} + 2 = 5.5$$

Hence,

$$R_B = 5.5 - 2.452 = -3.048 \text{ kN}$$

$$EI\frac{d^{2}y}{dx^{2}} = 2.452x - \frac{1}{7} \times x \times \frac{x}{2} \times \frac{x}{3} -2[x-5] -5[x-6]^{0}$$

$$EI\frac{dy}{dx} = \frac{2.45x^{2}}{2} - \frac{x^{4}}{4 \times 42} + A -\frac{2}{2}[x-5]^{2} -5[x-6]$$

$$EI\frac{dy}{dx} = 1.225x^{2} - \frac{x^{4}}{168} + A -[x-5]^{2} -5[x-6]$$
(1)
$$EIy = \frac{1.225x^{3}}{3} - \frac{x^{5}}{5 \times 168} + Ax + B -\frac{[x-5]^{3}}{3} -\frac{5}{2}[x-6]^{2}$$

$$EIy = 0.408x^{3} - \frac{x^{5}}{840} + Ax + B -\frac{[x-5]^{3}}{3} -\frac{5}{2}[x-6]^{2}$$
(2)

i.e.

or

At x = 0, y = 0, hence, *B* **= 0** 

At 
$$x = 7$$
 m,  $y = 0$ , hence,  $0 = 0.408(7)^3 - \frac{(7)^5}{840} + 7A - 2.667$ 

i.e. 
$$0 = 139.94 - 20.01 + 7A - 2.667$$

i.e. 
$$7A = 20.01 + 2.667 - 139.94 = -117.26$$

and 
$$A = -117.26/7 = -16.75$$

At 
$$x = 5$$
 m,  $\delta_c = \frac{1}{EI} \left\{ 0.408 (5)^3 - \frac{(5)^5}{840} + 5A \right\}$  from equation (2)

$$=\frac{1}{4300}\{51-3.72-83.75\}$$

i.e.

 $\delta_{C} = -8.48 \times 10^{-3} \,\mathrm{m}$ 

At 
$$x = 6$$
 m,  $\delta_D = \frac{1}{EI} \left\{ 0.408 (6)^3 - \frac{(6)^5}{840} + 6A \right\}$  from equation (2)  
 $= \frac{1}{4300} \{ 88.13 - 9.26 - 100.5 \}$ 

i.e.

$$\delta_D = -5.03 \times 10^{-3} \,\mathrm{m}$$

7. Determine the maximum deflection for the uniform-section beam shown, given that EI = 4300kN m<sup>2</sup>.

→ <del><</del> 1 m → <del><</del> 1 m →

Taking moments about *B* gives:

 $R_A \times 5 + 2 = 1 \times 3 \times 3.5 + 2 \times 2$ 

x = 0

3 m-

i.e.

 $5R_A = 10.5 + 4 - 2 = 12.5$ 

from which,

 $R_A = 12.5 / 5 = 2.5 \text{ kN}$ 

$$EI\frac{d^{2}y}{dx^{2}} = 2.5x - \frac{1 \times x^{2}}{2} \qquad -2[x-3] + \frac{1 \times [x-3]^{2}}{2} \qquad +2[x-4]^{0}$$

$$EI\frac{dy}{dx} = \frac{2.5x^{2}}{2} - \frac{x^{3}}{6} + A \qquad -\frac{2}{2}[x-3]^{2} + \frac{[x-3]^{3}}{6} \qquad +2[x-4] \qquad (1)$$

$$EIy = \frac{2.5x^{3}}{6} - \frac{x^{4}}{24} + Ax + B \qquad -\frac{[x-3]^{3}}{3} + \frac{[x-3]^{4}}{24} \qquad +\frac{2}{2}[x-4]^{2} \qquad (2)$$

At x = 0, y = 0, hence, *B* **= 0** 

At x = 5 m, y = 0, hence,  $0 = \frac{2.5(5)^3}{6} - \frac{(5)^4}{24} + 5A - \frac{(2)^3}{3} + \frac{(2)^4}{24} + \frac{2}{2}(1)^2$ 

i.e. 0 = 52.083 - 26.042 + 5A - 2.667 + 0.667 + 1

i.e. 5A = -52.083 + 26.042 + 2.667 - 0.667 - 1 = -25.041

and 
$$A = -25.041/5 = -5.008$$

For maximum deflection,  $\frac{dy}{dx} = 0$ 

Try the first span: 
$$0 = \frac{2.5x^2}{2} - \frac{x^3}{6} - 5.008$$

Solving using a calculator or smart phone gives:

x = 6.860 m (which is impossible) or x = 2.436 m or -1.80 m (which is impossible)

The value of 2.436 m is correct because it applies to the first quadrant – as the Macaulay bracket cannot be negative.

Hence, maximum deflection, 
$$\delta = \frac{1}{EI} \left( \frac{2.5x^3}{6} - \frac{x^4}{24} + 5.008x \right)$$
  
$$= \frac{1}{4300} \left( \frac{2.5(2.436)^3}{6} - \frac{(2.436)^4}{24} + 5.008(2.436) \right)$$
$$= \frac{1}{4300} (16.9308)$$

8. The beam CAB is simply supported at the points A and B and is subjected to a concentrated load W at the point C, together with a uniformly distributed load w between the points A and B, as shown. Determine the relationship between W and wl, so that no deflection will occur at the point B.





(1)

Taking moments about *B* gives:

$$R_A \times l = W\left(1.333l\right) + \frac{wl^2}{2}$$

 $R_A = 1.333W + \frac{wl}{2}$ 

i.e.

$$EI\frac{d^{2}y}{dx^{2}} = -Wx + R_{A}\left[x - \frac{l}{3}\right] - \frac{w}{2}\left[x - \frac{l}{3}\right]^{2} + R_{A}\left[x - \frac{l}{3}\right] - \frac{w}{2}\left[x - \frac{l}{3}\right]^{2} + \frac{R_{A}}{2}\left[x - \frac{l}{3}\right]^{2} - \frac{w}{6}\left[x - \frac{l}{3}\right]^{3} + \frac{R_{A}}{2}\left[x - \frac{l}{3}\right]^{2} - \frac{w}{6}\left[x - \frac{l}{3}\right]^{3} + \frac{R_{A}}{6}\left[x - \frac{l}{3}\right]^{3} - \frac{w}{24}\left[x - \frac{l}{3}\right]^{4}$$

At x = 0, y = 0, hence, B = 0

At 
$$x = \frac{l}{3}$$
,  $y = 0$ , hence,  $0 = -\frac{W\left(\frac{l}{3}\right)^3}{6} + A\left(\frac{l}{3}\right)$ 

or 
$$0 = -\frac{Wl^3}{162} + \frac{Al}{3}$$

from which, 
$$A = \frac{3W l^2}{162} = \frac{W l^2}{54}$$

At x = 1.333l, y = 0, hence,

$$0 = -\frac{W(1.333l)^{3}}{6} + 1.333\left(\frac{Wl^{2}}{54}\right) + \frac{l^{3}}{6}\left(1.333W + \frac{wl}{2}\right) - \frac{wl^{4}}{24}$$
$$0 = -0.395Wl^{3} + 0.0247l^{3}W + \frac{l^{3}}{6}\left(1.333W + \frac{wl}{2}\right) - \frac{wl^{4}}{24}$$

Dividing throughout by  $l^3$  gives:

$$0 = -0.395W + 0.0247W + \frac{1}{6} \left( 1.333W + \frac{wl}{2} \right) - \frac{wl^3}{24}$$
$$0 = -0.395W + 0.0247W + 0.222W + 0.0833wl - 0.04166wl$$

i.e.

i.e.

i.e.

$$0 = -0.1483W + 0.04164wl$$

from which,

$$w = \frac{-0.1483W}{0.0414l}$$

i.e.  $w = \frac{3.582W}{l}$ 

## EXERCISE 35, Page 164

**1.** Determine the position (from the left end) and the maximum deflection for the uniform-section beam shown, together with the reactions and end fixing forces by the double integration method.





$EI\frac{d^2y}{dx^2} = R_A x - M_A - \frac{0.7x^2}{2}$	$+\frac{0.7}{2}(x-1.5)^2$
$EI\frac{dy}{dx} = \frac{R_A x^2}{2} - M_A x - 0.1167 x^3 + A$	$+0.1167 (x - 1.5)^3$
$EIy = \frac{R_A x^3}{6} - \frac{M_A x^2}{2} - 0.292x^4 + Ax + B$	$+0.0292(x-1.5)^4$

At 
$$x = 0$$
,  $y = 0$ , hence,  $B = 0$   
At  $x = 0$ ,  $\frac{dy}{dx} = 09$ , hence,  $A = 0$   
At  $x = 3.5$ ,  $\frac{dy}{dx} = 0$   
hence,  $0 = 6.125 R_A - 3.5 M_A - 5 + 0.9336$   
or  $M_A = 1.75 R_A - 1.162$   
At  $x = 3.5$ ,  $y = 0$   
hence,  $0 = 7.146 R_A - 6.125 M_A - 4.382 + 0.4672$   
or  $M_A = 1.167 R_A - 0.6392$ 

(1)

(2)

Equating equations (1) and (2) gives:

 $(1.75 - 1.167) R_A = 1.162 - 0.6392$ 

and  $R_A = \frac{0.5228}{0.583}$ 

i.e.

*R<sub>A</sub>* = 0.897 kN

From equation (1),

 $M_A = 1.75(0.897) - 1.162 = 0.407$  kN m

 $R_B = (0.7 \times 1.5) - 0.897 = 0.153 \text{ kN}$ 

 $x = \frac{--0.1444 \pm \sqrt{(-0.1444)^2 - 4(0.2735)(-0.394)}}{2(0.2735)}$ 

Now,

and

$$M_B = 0.155 \text{ kN m}$$

*To find '\delta'*, try span CB:

$$0 = 0.4485x^{2} - 0.407x - 0.1167x^{3} + 0.1167(x^{3} - 3.375 + 2.25x - 1.5x^{2})$$

 $0 = 0.2735x^2 - 0.1444x - 0.394$ 

i.e.

= 1.49 m

This is not possible as 1.49 < 1.5

Try span AC:

 $0 = 0.4485x^2 - 0.407x - 0.1167x^3$ 

i.e.

$$0 = -0.1167x^2 + 0.4485x^2 - 0.407$$

and

$$x = \frac{--0.407 \pm \sqrt{(-0.407)^2 - 4(0.4885)(-0.1167)}}{2(0.4885)}$$

i.e x = 2.375 or x = 1.47 m which is OK

$$\delta = (0.4749 - 0.4397 - 0.1363)/EI$$

i.e.  $\delta = -0.101/EI$ 

2. Determine the end fixing moments and reactions for the encastré beam shown. The beam may be assumed to be of uniform section.



$EI\frac{d^2y}{dx^2} = R_A x - M_A = x \cdot \frac{x}{2} \cdot \frac{x}{3}$	$+\frac{3(x-3)^2}{2}+\frac{(x-3)^3}{6}$	$+5(x-4)^{0}$
$EI\frac{dy}{dx} = \frac{R_A x^2}{2} - M_A x - \frac{x^4}{24} + A$	$+\frac{3(x-3)^3}{6}+\frac{(x-3)^4}{24}$	+ 5 (x - 4)
@ $x = 0, \frac{dy}{dx} = 0$ hence, $A = 0$		
EIy = $\frac{R_A x^3}{6} - \frac{M_A x^2}{2} - \frac{x^5}{120} + B$	$+\frac{3(x-3)^4}{24}+\frac{(x-3)^5}{120}$	$+\frac{5(x-4)^2}{2}$

At x = 0, y = 0, hence, B = 0

At 
$$x = 5$$
,  $\frac{dy}{dx} = 0$ ,  
 $0 = 12.5 R_A - 5 M_A - 26.04 + 4 + 0.667 + 5$   
 $= 12.5 R_A - 5 M_A - 16.373$   
or  $R_A = 1.31 + 0.4 M_A$  (1)

At x = 5, y = 0,

$$0 = 20.833 R_A - 12.5 M_A - 26.04 + 2 + 0.27 + 2.5$$
$$= 20.833 R_A - 12.5 M_A - 21.27$$
(2)

Substituting equation (1) into equation (2) gives:

$$0 = 27.29 - 4.167 M_A - 21.27$$

from which,

$$\mathbf{M}_{\mathbf{A}} = \frac{6.02}{4.167} = \mathbf{1.445 \ kN \ m}$$
(3)

Substituting equation (3) into equation (1) gives:

$$R_A = 1.31 + 0.4(1.445) = 1.888 \text{ kN}$$

Resolving vertically gives:

$$R_A + R_B = \frac{3 \times 3}{2} = 4.5$$

from which,  $R_B = 4.5 - 1.888 = 2.612 \text{ kN}$ 

Taking moments about A gives:

$$M_B + 5 + \frac{3 \times 3}{2} \times 2 = R_B \times 5 + M_A$$

from which,

 $M_B = (2.612)(5) + 1.445 - 5 - 9 = 0.505$  kN m

3. Determine the end fixing moments and reactions for the uniform-section encastré beam shown.



$EI\frac{d^2y}{d^2} = R_A x - M_A - \frac{2x^2}{2} \qquad 11$	$-5(x-2) + \frac{(x-2)^2}{2}.2$	$(x-4)^{0}$
$EI\frac{dy}{dx} = \frac{R_A x^2}{2} - M_A x - \frac{x^3}{3} + A$	$-5\frac{(x-2)^2}{2} + \frac{(x-2)^3}{3}$	+ 10 (x - 4)
(a) $x = 0 \frac{dy}{dx} = 0$ hence $A = 0$		
EIy = $\frac{R_A x^3}{6} - \frac{M_A x^2}{2} - \frac{x^4}{12} + B$	$-5\frac{(x-2)^3}{6} + \frac{(x-2)^4}{12}$	$+\frac{10(x-4)^2}{2}$

At x = 0, y = 0, hence, B = 0

At 
$$x = 6$$
,  $\frac{dy}{dx} = 0$ ,

hence,

$$0 = 18 R_A - 6 M_A - 72 - 40 + 21.33 + 20$$

 $= 18 R_A - 6 M_A - 70.67$ 

or

$$R_A = 0.333 \, M_A + 3.926 \tag{1}$$

At x = 6, y = 0,

$$0 = 36 R_A - 18 M_A - 108 - 53.33 + 21.33 + 20$$

i.e.

$$0 = 36 R_A - 18 M_A - 120 \tag{2}$$

Substituting equation (1) into equation (2) gives:

$$0 = 12 M_A + 141.33 - 18 M_A - 120$$

and

$$M_A = 21.33/6 = 3.556 \text{ kN m}$$
 (3)

Substitute equation (3) into equation (1) gives:

 $R_A = 0.333(3.556) + 3.926 = 5.11 \text{ kN}$ 

Resolving vertically gives:

 $R_A + R_B = 2 \times 2 + 5$ from which,  $R_B = 9 - 5.11 = 3.89$  kN

Taking moments about A gives:

i.e.

i.e.

$$M_B + 10 + 5 \times 2 + 2 \times 2 \times 1 = R_B \times 6 + M_A$$

 $M_B = 3.89 \times 6 + 3.556 - 10 - 10 - 4$ 

 $M_B = 2.896 \text{ kN m}$ 

**4.** Determine the position (from the left end) and the maximum deflection for the uniform-section beam shown, together with the reactions and end fixing forces.



$$EI\frac{d^{2}y}{dx^{2}} = R_{A}x - M_{A} - \frac{0.7x^{2}}{2} + \frac{0.7}{2}[x-2]^{2}$$
$$EI\frac{dy}{dx} = \frac{R_{A}x^{2}}{2} - M_{A}x - \frac{0.7x^{3}}{6} + A + \frac{0.7}{6}[x-2]^{3}$$

At 
$$x = 0$$
,  $\frac{dy}{dx} = 0$ , hence,  $A = 0$   

$$EIy = \frac{R_A x^3}{6} - \frac{M_A x^2}{2} - \frac{0.7x^4}{24} + B + \frac{0.7}{24} [x - 2]^4$$

At x = 0, y = 0, hence, *B* **= 0** 

At x = 5 m,  $\frac{dy}{dx} = 0$ 

Hence,

$$0 = \frac{R_A(5)^2}{2} - M_A(5) - \frac{0.7(5)^3}{6} + \frac{0.7}{6} [5-2]^3$$

i.e.

 $0 = 12.5R_A - 5M_A - 14.583 + 3.15$ 

or

$$5M_A = 12.5R_A - 11.433$$

and

$$M_A = 2.5R_A - 2.2866 \tag{1}$$

At x = 5 m, y = 0

Hence, 
$$0 = \frac{R_A(5)^3}{6} - \frac{M_A(5)^2}{2} - \frac{0.7(5)^4}{24} + \frac{0.7}{24} [5-2]^4$$

i.e.

$$0 = 20.833R_A - 12.5M_A - 18.229 + 2.363$$

or

$$12.5M_A = 20.833R_A - 15.866$$

i.e.  $M_A = 1.6666R_A - 1.2693$ Equating equations (1) and (2) gives:

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(2)

i.e. 
$$R_A (2.5 - 1.66666) = 2.2866 - 1.2693$$

i.e.  $0.8334R_A = 1.0173$ 

and

i.e.

$$\boldsymbol{R}_{A} = \frac{1.0173}{0.8334} = \mathbf{1.221} \, \mathbf{kN} \tag{3}$$

Substituting equation (3) into equation (1) gives:

$$M_A = 2.5R_A - 2.2866$$
  
= 2.5(1.221) - 2.2866  
 $M_A = 0.766 \text{ kN m}$  (4)

Taking moments about *B* gives:

i.e. 
$$R_{A} \times 5 = 0.7 \times 2 \times 4 + M_{A} - M_{B}$$
$$5R_{A} = 5.6 + M_{A} - M_{B}$$
(5)

Substituting equations (3) and (4) into equation (5) gives:

and  $M_B = 5.6 + 0.766 - M_B$ i.e.  $M_B = 0.261$  kN m (6)

 $R_A + R_B = 0.7 \times 2$ 

Resolving vertically gives:

and from equation (3),  $1.221 + R_B = 1.4$ from which,  $R_B = 1.4 - 1.221 = 0.179$  kN For maximum deflection,  $\frac{dy}{dx} = 0$ ,

i.e. 
$$0 = \frac{R_A x^2}{2} - M_A x - \frac{0.7 x^3}{6} + \frac{0.7}{6} [x - 2]^3$$

i.e. 
$$0 = \frac{(1.221)x^2}{2} - 0.766x - \frac{0.7x^3}{6} + \frac{0.7}{6} \left(x^3 - 6x^2 + 12x - 8\right)$$

i.e. 
$$0 = 0.6105x^2 - 0.766x - 0.1167x^3 + 0.1167x^3 - 0.7x^2 + 1.4x - 0.9333$$

i.e. 
$$-0.0895x^2 + 0.634x - 0.9333 = 0$$

Using a calculator or the quadratic formula,

x = 2.087 m or 4.997 m (which is ignored)

Hence, maximum deflection,

$$\delta = \frac{1}{EI} \left\{ \frac{R_A x^3}{6} - \frac{M_A x^2}{2} - \frac{0.7 x^4}{24} + B + \frac{0.7}{24} [x - 2]^4 \right\}$$
$$= \frac{1}{EI} \left\{ \frac{(1.221)(2.087)^3}{6} - \frac{(0.766)(2.087)^2}{2} - \frac{0.7(2.087)^4}{24} + \frac{0.7}{24} [2.087 - 2]^4 \right\}$$
$$\delta = -\frac{0.372}{EI}$$

i.e.

$$=-\frac{\partial e_{I}}{EI}$$

5. Determine the end fixing moments and reactions for the encastré beam shown. The beam may be assumed to be of uniform section.





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$$\frac{w}{x} = \frac{3}{4} \quad \text{i.e.} \quad w = 0.75x$$

$$EI \frac{d^{2}y}{dx^{2}} = R_{d}x - M_{d} - 0.75x \times \frac{x}{2} \times \frac{x}{3}$$

$$\frac{3}{4}[x-4] \qquad 5[x-5]$$

$$\frac{[x-4]}{2} \times \frac{[x-4]}{3}$$

$$\frac{3}{4}[x-4] \qquad 5[x-5]$$

$$\frac{[x-4]}{2} \times \frac{[x-4]}{3}$$

$$\frac{[x-4]}{2} \times \frac{[x-4]}{3}$$

$$\frac{[x-4]}{2} \times \frac{[x-4]}{3}$$

$$\frac{[x-4]}{2} \times \frac{[x-4]}{3}$$

$$\frac{[x-4]}{4 \times 6} + [x-4]^{3} \times 0.5 \quad 5[x-5]$$

$$At x = 0, \ \frac{dy}{dx} = 0, \text{ hence, } A = 0$$

$$EI \frac{dy}{dx} = \frac{R_{d}x^{2}}{2} - M_{d}x - \frac{0.75x^{4}}{24}$$

$$+ \frac{[x-4]^{4}}{32} + 0.5[x-4]^{3} \quad 5[x-5] \quad (1)$$

$$EJy = \frac{R_{d}x^{3}}{6} - \frac{M_{d}x^{2}}{2} - \frac{0.75x^{5}}{24 \times 5} + B$$

$$+ \frac{[x-4]^{5}}{160} + \frac{[x-4]^{4}}{8} \qquad \frac{5[x-5]^{2}}{2}$$

$$At x = 0, y = 0, \text{ hence, } B = 0$$

$$EIy = \frac{R_{d}x^{3}}{6} - \frac{M_{d}x^{2}}{2} - \frac{x^{5}}{160}$$

$$+ \frac{[x-4]^{5}}{160} + \frac{[x-4]^{4}}{8} \qquad 2.5[x-5]^{2} \quad (2)$$

At 
$$x = 6$$
 m,  $y = 0$ , hence,

$$0 = \frac{R_A(6)^3}{6} - \frac{M_A(6)^2}{2} - \frac{(6)^5}{160} + \frac{(2)^5}{160} + \frac{(2)^4}{8} + 2.5(1)^2$$

i.e.

$$0 = 36R_A - 18M_A - 48.6 + 0.2 + 2 + 2.5$$

i.e.

$$18M_A = 36R_A - 43.9$$

 $M_A = 2R_A - 2.439$ 

or

At 
$$x = 6$$
 m,  $\frac{dy}{dx} = 0$ , hence,

$$x = 6 \text{ m}, \frac{dy}{dx} = 0, \text{ hence,}$$

$$0 = \frac{R_A(6)^2}{2} - 6M_A - \frac{0.75(6)^4}{24} + \frac{[6-4]^4}{32} + 0.5[6-4]^3 + 5[6-5]$$
$$0 = 18R_A - 6M_A - 40.5 + 0.5 + 4 + 5$$

(3)

i.e.

i.e.  $6M_A = 18R_A - 31$ 

or

$$M_A = 3R_A - 5.167$$

(4)

Equating equations (3) and (4) gives:

$$2R_A - 2.439 = 3R_A - 5.167$$

from which,  $R_A = 5.167 - 2.439 = 2.728 \text{ kN}$ 

From equation (4),  $M_A = 3R_A - 5.167$ 

$$= 3(2.728) - 5.167$$

i.e.  $M_A = 3.017 \text{ kN}$ 

Resolving vertically gives:

 $R_A + R_B = 0.75 \times 4 \times \frac{4}{2} = 6$ 

Hence,

 $R_{B} = 6 - 2.728 = 3.272 \text{ kN}$ 

Taking moments about *B* gives:

 $R_A \times 6 + 5 = M_A - M_B + \frac{3 \times 4}{2} \times \left(\frac{4}{3} + 2\right)$ i.e.  $2.728 \times 6 + 5 = 3.017 - M_B + 20$ i.e.  $M_B = 3.017 + 20 - 2.728 \times 6 - 5$ i.e.  $M_B = 1.649 \text{ kN}$ 



$$w = 2$$

$$EI \frac{d^{2}y}{dx^{2}} = R_{A}x - M_{A} - 02x \times \frac{x}{2}$$

$$-5[x-3]$$

$$+\frac{2}{2}[x-3]^{2}$$

$$10[x-6]$$

$$EI \frac{dy}{dx} = \frac{R_{A}x^{2}}{2} - M_{A}x - \frac{x^{3}}{3} + A$$

$$-\frac{5}{2}[x-3]^{2} + \frac{[x-3]^{3}}{3}$$

$$\frac{10}{2}[x-6]^{2}$$
(1)
$$At x = 0, \frac{dy}{dx} = 0, \text{ hence, } A = 0$$

$$EIy = \frac{R_{A}x^{3}}{6} - \frac{M_{A}x^{2}}{2} - \frac{x^{4}}{12} + B$$

$$-\frac{5}{2}[x-3]^{3} + \frac{[x-3]^{4}}{12}$$

$$\frac{5}{3}[x-6]^{3}$$
(2)

At x = 0, y = 0, hence, **B = 0** 

At 
$$x = 6$$
 m,  $\frac{dy}{dx} = 0$ , hence,

i.e.

$$0 = 18R_A - 6M_A - 72 - 22.5 + 9$$

 $M_A = 3R_A - 14.25$ 

i.e.

$$6M_A = 18R_A - 85.5$$

or

At x = 6 m, y = 0, hence,

$$0 = \frac{R_A(6)^3}{6} - M_A \times \frac{36}{2} - \frac{(6)^4}{12} - \frac{5(3)^3}{6} + \frac{(3)^3}{12}$$

 $0 = \frac{R_A(6)^2}{2} - M_A(6) - \frac{(6)^3}{3} - \frac{5}{2} \times 3^2 + \frac{(3)^3}{3} + 0$ 

i.e.

$$0 = 36R_A - 18M_A - 108 - 22.5 + 6.75$$

i.e.  $18M_A = 36R_A - 123.75$ 

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(3)

$$M_A = 2R_A - 6.875$$

(4)

(5)

Equating equations (3) and (4) gives:

$$3R_A - 14.25 = 2R_A - 6.875$$

from which,  $R_A = 14.25 - 6.875 = 7.375 \text{ kN}$ 

From equations (4) and (5),

= 2(7.375) - 6.875

 $M_A = 2R_A - 6.875$ 

i.e.

$$M_A = 7.875 \text{ kN}$$
 (6)

Resolving vertically gives:

 $R_A + R_B = 2 \times 3 + 5 = 11$ 

Hence,

$$R_B = 11 - 7.375 = 3.625 \text{ kN}$$

Taking moments about *B* gives:

	$R_A \times 9 + 10 + M_B = M_A + 2 \times 3 \times 7.5 + 5 \times 6$
i.e.	$7.375 \times 9 + 10 + M_{B} = 7.875 + 45 + 30$
i.e.	$M_{B} = 7.875 + 45 + 30 - 7.375 \times 9 - 10$

i.e.  $M_B = 6.50 \text{ kN}$ 

# EXERCISE 36, Page 166





$$x\frac{dy}{dx} - y = \frac{1}{E} \times \text{ moment of area of the } M/I \text{ diagram about } A$$

$$\left[\left(2l\theta_B - y_B\right) - \left(0 \times \theta_A - y_A\right)\right] = -\frac{1}{E} \left[\frac{Wl}{I} \times \frac{2}{3} \times l \times \frac{l}{2} + \frac{Wl}{2I} \times \frac{3l}{2} \times l + \frac{Wl}{2I} \times \frac{l}{2} \times \left(l + \frac{2l}{3}\right)\right]$$

$$\theta_{B} = y_{B} = 0$$
, hence,  $y_{A} = -\frac{W l^{3}}{EI} \left[ \frac{1}{3} + \frac{3}{4} + \frac{1}{4} \left( \frac{5}{3} \right) \right]$ 

i.e. maximum deflection,  $y_A = -\frac{3W l^3}{2EI}$ 

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or